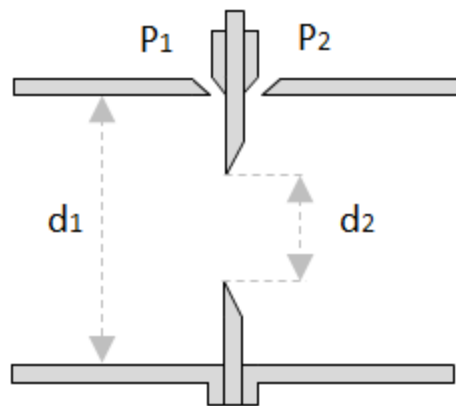


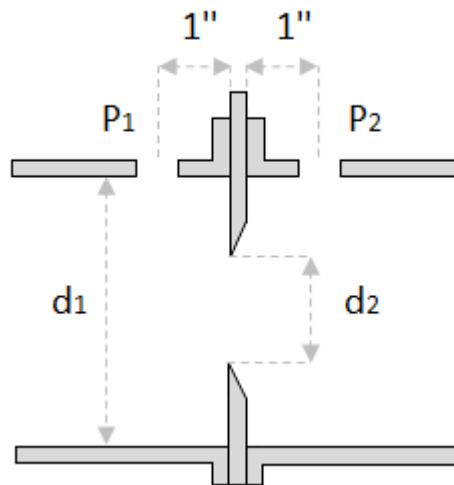
# Large Diameter Orifice Flow Meter For Gases

This application determines the flowrate through a large diameter orifice meter using the equations defined in ISO 5167

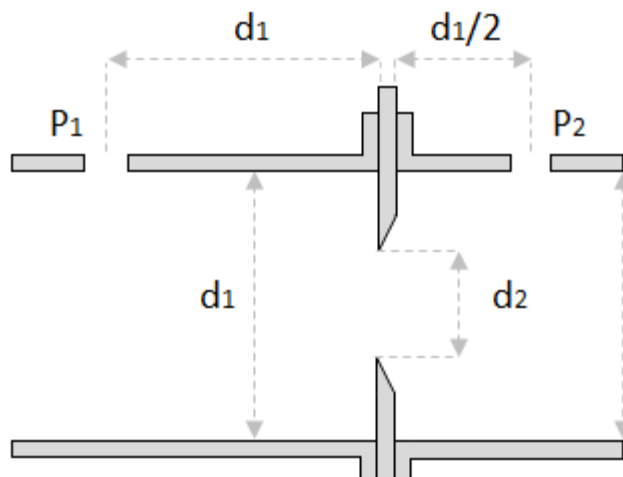
Corner taps



Flange taps



D-D/2 taps



Recommended parameters:

For all taps

$$d_2 \geq 1.25 \text{ cm}$$

$$5 \text{ cm} \leq d_1 \leq 1 \text{ m}$$

$$0.1 \leq d_2/d_1 \leq 0.75$$

Corner and D-D/2 taps

$$Re_y \geq 4000 \text{ for } 0.1 \leq d_2/d_1 \leq 0.5$$

$$Re_y \geq 16000 (d_2/d_1)^2 \text{ for } d_2/d_1 > 0.5$$

Flange taps

$$Re_y \geq 4000$$

$$Re_y \geq 170000 D (d_2/d_1)^2 \text{ where } D \text{ is in meters}$$

Expansibility equation is valid for pressure ratio  $P_2/P_1 \geq 0.75$

Reference:

ISO 5167-1:2003. Measurement of fluid flow by means of pressure differential devices inserted in circular cross-section conduits running full

## Parameters

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Tap type ("corner",  
"flange" or "D-D/2")

$$\text{taptype} := \text{"flange"}$$

Gas

$$\text{gas} := \text{"air"}$$

Temperature

$$T := 313$$

Upstream pressure

$$P_1 := 111000$$

Density

$$\rho := \text{ThermophysicalData:Property}(\text{density, gas, temperature} = T, \text{pressure} = P_1)$$

$$\rho = 1.236$$

Viscosity

$$\mu := \text{ThermophysicalData:Property}(\text{viscosity, gas, temperature} = T, \text{pressure} = P_1)$$

$$\mu = 1.916 \times 10^{-5}$$

Differential pressure  $\Delta P := P_1 - 103000 = 8000$

Pressure ratio  $PR := \frac{P_1 - \Delta P}{P_1} = 0.928$

Isentropic expansion coefficient  $K := \frac{\text{ThermophysicalData:Property}(C_{p\text{mass}}, \text{gas}, \text{temperature} = T, \text{pressure} = P_1)}{\text{ThermophysicalData:Property}(C_{v\text{mass}}, \text{gas}, \text{temperature} = T, \text{pressure} = P_1)}$

$$K = 1.401$$

Pipe diameter  $d_1 := 0.075$

Orifice diameter  $d_2 := 0.01$

Standard temperature and pressure  $T_{\text{std}} := 288.9$

$$P_{\text{std}} := 101325$$

## Equations

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Throat area  $A_{\text{throat}} := \frac{\pi \cdot d_2^2}{4} = 7.854 \times 10^{-5}$

Pipe area  $A_{\text{pipe}} := \frac{\pi \cdot d_1^2}{4} = 0.004$

Diameter ratio  $\beta := \frac{d_2}{d_1} = 0.133$

Discharge coefficient

$$C_{d_{base}} := 0.5961 + 0.0261 \cdot \beta^2 - 0.216 \cdot \beta^8 + 0.000521 \cdot \left( \frac{10^6 \cdot \beta}{Rey} \right)^{0.7} +$$

$$\left( 0.0188 + 0.0063 \cdot \left( \frac{19000 \cdot \beta}{Rey} \right)^{0.8} \right) \cdot \left( \frac{10^6}{Rey} \right)^{0.3} \cdot \beta^{3.5} +$$

$$\left( 0.043 + 0.08 \cdot e^{-10 \cdot L_1} - 0.123 \cdot e^{-7 \cdot L_1} \right) \cdot \left( 1 - 0.11 \cdot \left( \frac{19000 \cdot \beta}{Rey} \right)^{0.8} \right) \cdot \frac{\beta^4}{1 - \beta^4} -$$

$$0.031 \cdot \left( \frac{2 \cdot L_2}{1 - \beta} - 0.8 \cdot \left( \frac{2 \cdot L_2}{1 - \beta} \right)^{1.1} \right) \cdot \beta^{1.3}$$

$$C_{d_{base}} := \begin{cases} C_{d_{base}} + 0.011 \cdot (0.75 - \beta) \cdot \left( 2.8 - \frac{d_1}{0.0254} \right) & d_1 < 0.07112 \\ C_{d_{base}} & \text{otherwise} \end{cases}$$

$$L_1 := \begin{cases} 0 & \text{tatype} = \text{"corner"} \\ \frac{0.0254}{d_1} & \text{tatype} = \text{"flange"} \\ 1 & \text{tatype} = \text{"D-D/2"} \end{cases} \quad L_2 := \begin{cases} 0 & \text{tatype} = \text{"corner"} \\ \frac{0.0254}{d_1} & \text{tatype} = \text{"flange"} \\ 0.47 & \text{tatype} = \text{"D-D/2"} \end{cases}$$

$$\text{DragCoeff} := Cd = C_{d_{base}}$$

Gas expansion factor (Buckingham equation)

$$e := 1 - \left( 0.41 + 0.35 \cdot \beta^4 \right) \cdot \frac{\Delta P}{K \cdot P_1} = 0.979$$

Mass flowrate

$$\text{MassFlowrate} := Q_m = \frac{e \cdot Cd \cdot A_{throat} \cdot \sqrt{2 \cdot \rho \cdot \Delta P}}{\sqrt{1 - \beta^4}} = Q_m = 0.011 \cdot Cd$$

Gas velocity

$$V_{pipe} := \frac{Q_m}{A_{pipe} \cdot \rho} = 183.175 \cdot Q_m$$

Reynolds number

$$\text{Reynolds} := Rey = \frac{V_{pipe} \cdot d_1 \cdot \rho}{\mu} = Rey = 8.861 \times 10^5 \cdot Q_m$$

## Numerical Solution and Results

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Equations  $\text{eqs} := \{\text{DragCoeff}, \text{MassFlowrate}, \text{Reynolds}\}$

Parameters to solve for  $\text{vars} := \text{indets}(\text{eqs}, \text{name}) = \{\text{Cd}, \text{Q}_m, \text{Rey}\}$

Numerical solution  $\text{res} := \text{fsolve}(\text{eqs}, \text{vars}) = \{\text{Cd} = 0.601, \text{Q}_m = 0.006, \text{Rey} = 5.758 \times 10^3\}$

$$\text{Cd} := \text{eval}(\text{Cd}, \text{res}) = 0.601$$

$$\text{Q}_m := \text{eval}(\text{Q}_m, \text{res}) = 0.006$$

$$\text{Rey} := \text{eval}(\text{Rey}, \text{res}) = 5.758 \times 10^3$$

Static pressure loss from a distance  $d_1$  upstream and  $6 d_1$  downstream of the orifice

$$w := \frac{\sqrt{1 - \beta^4} - \text{Cd} \cdot \beta^2}{\sqrt{1 - \beta^4} + \text{Cd} \cdot \beta^2} \cdot \Delta P = 7.831 \times 10^3$$

Minor loss coefficient  $K_m := \frac{2 \cdot w}{\rho \cdot V_{\text{pipe}}^2} = 8.946 \times 10^3$

Volumetric flowrate  $Q_a := \frac{Q_m}{\rho} = 0.005$

Volumetric flowrate at standard conditions  $Q_s := Q_a \cdot \frac{P_1 \cdot T_{\text{std}}}{P_{\text{std}} \cdot T} = 0.005$