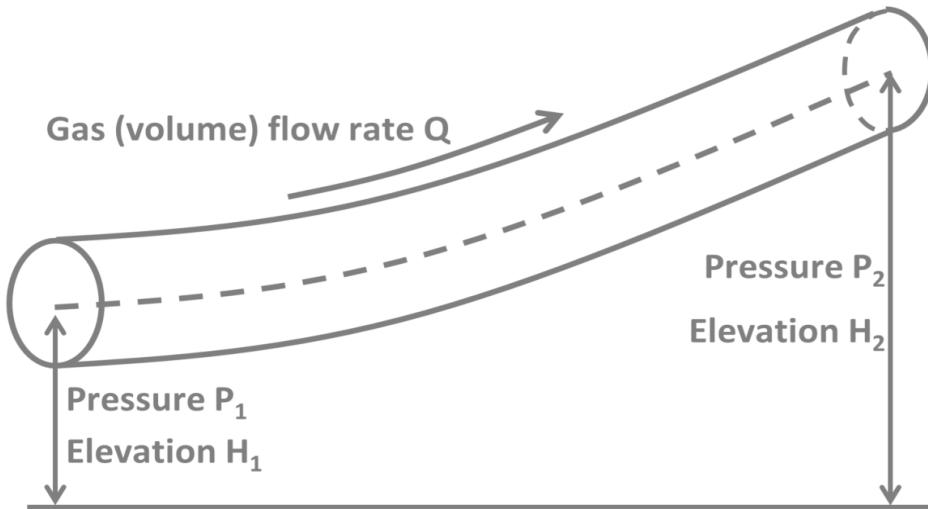


Natural gas pipeline sizing (USCS)

This application calculate Gas flow rate as Natural gas pipeline sizing calculation. This calculation is based on General flow equation, AGA, Weymouth, Panhandle A , Panhandle B, and IGT equation. And, U.S. Customary System of units is used in this application.



Reference : Gas Pipeline Hydraulics, E. Shashi Menon, 2005

Design parameters

In this section, the gas properties and the geometrical parameters are defined for the calculation later.

Gas properties

$$\text{Pipeline Inlet pressure } P_1 := 999.99 \text{ psi}$$

$$\text{Pipeline outlet pressure } P_2 := 800.00 \text{ psi}$$

$$\text{Gas pressure at Base condition } P_b := 14.7 \text{ psi}$$

$$\text{Gas temperature at Base condition } T_{b_F} := 60 \text{ degF}$$

$$\text{Specific Gravity } G := 0.6$$

$$\text{Average gas flowing temperature } T_{f_F} := 70 \text{ degF}$$

Pipeline parameters

Pipe Length	$L := 10 \text{ mile}$
Pipe inside diameter	$D_p := 19.00 \text{ inch}$
Pipe roughness	$\epsilon := 0.0007 \text{ inch}$
Upstream elevation	$H_1 := 10 \text{ ft}$
Downstream elevation	$H_2 := 110 \text{ ft}$
Pipe efficiency (A decimal value less than or equal to 1.0)	$E := 0.95$

Gas properties

Density, viscosity and compressibility factor of gas can be obtained with the fluid properties specified in the previous section.

Average gas temperature in Rankine	$T_{f_R} := \text{temperature_conversion}(T_{f_F}, \text{"degF"}, \text{"degR"}) = 529.67 \text{ }^{\circ}\text{R}$
Gas temperature at Base condition in Rankine	$T_{b_R} := \text{temperature_conversion}(T_{b_F}, \text{"degF"}, \text{"degR"}) = 519.67 \text{ }^{\circ}\text{R}$

Note:

The unit of temperature can be converted with `temperature_conversion()` function defined in the Code region.

Average gas pressure	$P_{avg} := \frac{2}{3} \cdot \left(P_1 + P_2 - \frac{P_1 \cdot P_2}{P_1 + P_2} \right) = 903.698 \text{ psi}$
Compressibility factor (CNGA method)	$Z := \frac{1}{\frac{P_{avg}}{\text{psi}} \cdot 344400 \cdot 10^{1.785 \cdot G} + \left(\frac{T_{f_R}}{\text{degR}} \right)^{3.825}} = 877.53 \times 10^{-3}$
Viscosity	$\mu := 0.0126 \text{ centipoise}$

Gas flow rate calculation

Gas (volume) flow rate can be calculated with several methods. In this section, these calculations are shown.

General flow equation with Colebrook-White equation of Friction factor

Volume flow rate

$$Q_{GF} := 77.54 \cdot E \cdot \left(\frac{\frac{T_b \cdot R}{degR}}{\frac{P_b}{psi}} \right) \cdot \left(\frac{\left(\frac{P_1}{psi} \right)^2 - \left(\frac{P_2}{psi} \right)^2}{G \cdot \left(\frac{T_f \cdot R}{degR} \right) \cdot \left(\frac{L}{mile} \right) \cdot Z \cdot f} \right)^{0.5} \cdot \left(\frac{D_p}{inch} \right)^{2.5}$$

Reynolds number

$$Rey_{GF} := 0.0004778 \cdot \left(\frac{\frac{P_b}{psi}}{\frac{T_b \cdot R}{degR}} \right) \cdot \left(\frac{\frac{G \cdot Q_{GF}}{D_p}}{\frac{\mu}{lb \cdot ft \cdot s} \cdot \frac{D_p}{inch}} \right)$$

By using above 2 equations, the friction factor can be obtained based on Colebrook-white equation. And, the final result of Gas flow rate and Reynolds number also can be calculated.

Friction factor

$$f_{GF_res} := fsolve \left(\frac{1}{\sqrt{f}} = -2 \cdot \log10 \left(\frac{\epsilon}{3.7 \cdot D_p} + \frac{2.51}{Rey_{GF} \cdot \sqrt{f}} \right), f \right) = 10.17 \times 10^{-3}$$

Volume flow rate

$$Q_{GF_res} := 77.54 \cdot E \cdot \left(\frac{\frac{T_b \cdot R}{degR}}{\frac{P_b}{psi}} \right) \cdot \left(\frac{\left(\frac{P_1}{psi} \right)^2 - \left(\frac{P_2}{psi} \right)^2}{G \cdot \left(\frac{T_f \cdot R}{degR} \right) \cdot \left(\frac{L}{mile} \right) \cdot Z \cdot f_{GF_res}} \right)^{0.5} \cdot \left(\frac{D_p}{inch} \right)^{2.5} \cdot \frac{ft^3}{day}$$

$$Q_{GF_res} = 461.605 \frac{1000000 \text{ ft}^3}{d}$$

$$Rey_{GF_res} := 0.0004778 \cdot \left(\frac{\frac{P_b}{psi}}{\frac{T_b \cdot R}{degR}} \right) \cdot \left(\frac{\frac{G \cdot \frac{Q_{GF_res}}{ft^3}}{day}}{\frac{\mu}{lb \cdot ft \cdot s} \cdot \frac{D_p}{inch}} \right) = 2.327 \times 10^7$$

General flow equation with American Gas Association (AGA) equation of Transmission factor

Pipe drag factor

$$D_f := 0.95$$

Volume flow rate

$$Q_{AGA} := 77.54 \cdot E \cdot \left(\frac{\frac{T_b \cdot R}{degR}}{\frac{P_b}{psi}} \right) \cdot \left(\frac{\left(\frac{P_1}{psi} \right)^2 - \left(\frac{P_2}{psi} \right)^2}{G \cdot \left(\frac{T_f \cdot R}{degR} \right) \cdot \left(\frac{L}{mile} \right) \cdot Z \cdot f} \right)^{0.5} \cdot \left(\frac{D_p}{inch} \right)^{2.5}$$

$$Rey_{AGA} := 0.0004778 \cdot \left(\frac{\frac{P_b}{psi}}{\frac{T_b \cdot R}{degR}} \right) \cdot \left(\frac{G \cdot Q_{AGA}}{\frac{\mu}{lb \cdot ft \cdot s} \cdot \frac{D_p}{inch}} \right)$$

Von Karman smooth pipe transmission factor

$$F_t_{res} := \text{solve} \left(F_t = 4 \cdot \log_{10} \left(\frac{Rey_{AGA}}{F_t} \right) - 0.6, F_t \right)$$

Transmisson factor

$$F_{AGA} := \min \left(4 \cdot \log_{10} \left(\frac{3.4 \cdot D_p}{\epsilon} \right), 4 \cdot D_f \cdot \log_{10} \left(\frac{Rey_{AGA}}{1.4125 \cdot F_t_{res}} \right) \right)$$

Therefore, friction factor can be obtained with above equations, and Gas flow rate and Reynolds number can be calculated as follow.

Friction factor

$$f_{AGA} := \text{solve} \left(F_{AGA} = \frac{2}{\sqrt{f}}, f \right) = 10.14 \times 10^{-3}$$

Volume flow rate

$$Q_{AGA_res} := 77.54 \cdot E \cdot \left(\frac{\frac{T_b \cdot R}{degR}}{\frac{P_b}{psi}} \right) \cdot \left(\frac{\left(\frac{P_1}{psi} \right)^2 - \left(\frac{P_2}{psi} \right)^2}{G \cdot \left(\frac{T_f \cdot R}{degR} \right) \cdot \left(\frac{L}{mile} \right) \cdot Z \cdot f_{AGA}} \right)^{0.5} \cdot \left(\frac{D_p}{inch} \right)^{2.5} \cdot \frac{ft^3}{day}$$

$$Q_{AGA_res} = 462.311 \frac{1000000 \text{ ft}^3}{d}$$

Reynolds number

$$Rey_{AGA} := 0.0004778 \cdot \left(\frac{\frac{P_b}{psi}}{\frac{T_b \cdot R}{degR}} \right) \cdot \left(\frac{G \cdot \frac{Q_{AGA_res}}{ft^3 \cdot day}}{\frac{\mu}{lb \cdot ft \cdot s} \cdot \frac{D_p}{inch}} \right) = 2.330 \times 10^7$$

Weymouth equation

Elevation adjustment parameter

$$s_{el} := 0.0375 \cdot G \cdot \left(\frac{\frac{H_2}{ft} - \frac{H_1}{ft}}{\frac{T_f R}{degR} \cdot Z} \right) = 0.005$$

Equivalent length

$$L_e := \frac{L \cdot \left(e^{s_{el}} - 1 \right)}{s_{el}} = 10.024 \text{ mi}$$

Flow velocity

$$Q_w := 433.5 \cdot E \cdot \left(\frac{\frac{T_b R}{degR}}{\frac{P_b}{psi}} \right) \cdot \left(\frac{\left(\frac{P_1}{psi} \right)^2 - e^{s_{el}} \cdot \left(\frac{P_2}{psi} \right)^2}{G \cdot \left(\frac{T_f R}{degR} \right) \cdot \left(\frac{L_e}{mile} \right) \cdot Z} \right)^{0.5} \cdot \left(\frac{D_p}{inch} \right)^{2.667} \cdot \frac{ft^3}{day}$$

$$Q_w = 423.235 \frac{1000000 \text{ ft}^3}{d}$$

Transmission factor

$$F_w := 11.18 \cdot \left(\frac{D_p}{inch} \right)^{\frac{1}{6}} = 18.263$$

Friction factor

$$f_w := \text{solve} \left(F_w = \frac{2}{\sqrt{f}}, f \right) = 11.99 \times 10^{-3}$$

Panhandle A equation

Elevation adjustment parameter

$$s_{el} := 0.0375 \cdot G \cdot \left(\frac{\frac{H_2}{ft} - \frac{H_1}{ft}}{\frac{T_f R}{degR} \cdot Z} \right) = 0.005$$

Equivalent length

$$L_e := \frac{L \cdot \left(e^{s_{el}} - 1 \right)}{s_{el}} = 10.024 \text{ mi}$$

Flow velocity

$$Q_{pA} := 435.87 \cdot E \cdot \left(\frac{\frac{T_b R}{degR}}{\frac{P_b}{dsi}} \right)^{1.0788} \cdot \left(\frac{\left(\frac{P_1}{psi} \right)^2 - e^{s_{el}} \cdot \left(\frac{P_2}{psi} \right)^2}{G^{0.8539} \cdot \left(\frac{T_f R}{degR} \right) \cdot \left(\frac{L_e}{mile} \right) \cdot Z} \right)^{0.5394} \cdot \left(\frac{D_p}{inch} \right)^{2.6182} \cdot \frac{ft^3}{day}$$

$$Q_{pA} = 567.618 \frac{1000000 \text{ ft}^3}{d}$$

Transmission factor

$$F_{pA} := 7.2111 \cdot E \cdot \left(\frac{\left(\frac{Q_{pA}}{\frac{ft^3}{d}} \right) \cdot G}{\frac{D_p}{inch}} \right)^{0.07305} = 23.205$$

Friction factor

$$f_{pA} := \text{solve}\left(F_{pA} = \frac{2}{\sqrt{f}}, f\right) = 7.43 \times 10^{-3}$$

Panhandle B equation

Elevation adjustment parameter

$$s_{el} := 0.0375 \cdot G \cdot \left(\frac{\frac{H_2}{ft} - \frac{H_1}{ft}}{\frac{T_f R}{degR} \cdot Z} \right) = 0.005$$

Equivalent length

$$L_e := \frac{L \cdot \left(e^{s_{el}} - 1 \right)}{s_{el}} = 10.024 \text{ mi}$$

Flow velocity

$$Q_{pB} := 737 \cdot E \cdot \left(\frac{\frac{T_b R}{degR}}{\frac{P_b}{psi}} \right)^{1.02} \cdot \left(\frac{\left(\frac{P_1}{psi} \right)^2 - e^{s_{el}} \cdot \left(\frac{P_2}{psi} \right)^2}{G^{0.961} \cdot \left(\frac{T_f R}{degR} \right) \cdot \left(\frac{L_e}{mile} \right) \cdot Z} \right)^{0.51} \cdot \left(\frac{D_p}{inch} \right)^{2.53} \cdot \frac{ft^3}{day}$$
$$Q_{pB} = 536.397 \frac{1000000 \text{ ft}^3}{d}$$

Transmission factor

$$F_{pB} := 16.7 \cdot E \cdot \left(\frac{\left(\frac{Q_{pB}}{\frac{ft^3}{d}} \right) \cdot G}{\frac{D_p}{inch}} \right)^{0.01961} = 21.989$$

Friction factor

$$f_{pB} := \text{solve}\left(F_{pB} = \frac{2}{\sqrt{f}}, f\right) = 8.27 \times 10^{-3}$$

Institute of Gas Technology (IGT) equation

Elevation adjustment parameter

$$s_{el} := 0.0375 \cdot G \cdot \left(\frac{\frac{H_2}{ft} - \frac{H_1}{ft}}{\frac{T_f R}{degR} \cdot Z} \right) = 0.005$$

Equivalent length

$$L_e := \frac{L \cdot (e^{s_{el}} - 1)}{s_{el}} = 10.024 \text{ mi}$$

Flow velocity

$$Q_{IGT} := 136.9 \cdot E \cdot \left(\frac{\frac{T_b R}{degR}}{\frac{P_b}{psi}} \right) \cdot \left(\frac{\left(\frac{P_1}{psi} \right)^2 - e^{s_{el}} \cdot \left(\frac{P_2}{psi} \right)^2}{G^{0.8} \cdot \left(\frac{T_f R}{degR} \right) \cdot \left(\frac{L_e}{mile} \right) \cdot \left(\frac{\mu}{lb \cdot ft \cdot s} \right)^{0.2}} \right)^{0.555} \cdot \left(\frac{D_p}{inch} \right)^{2.667} \cdot \frac{ft^3}{day}$$

$$Q_{IGT} = 560.708 \frac{1000000 \text{ ft}^3}{d}$$